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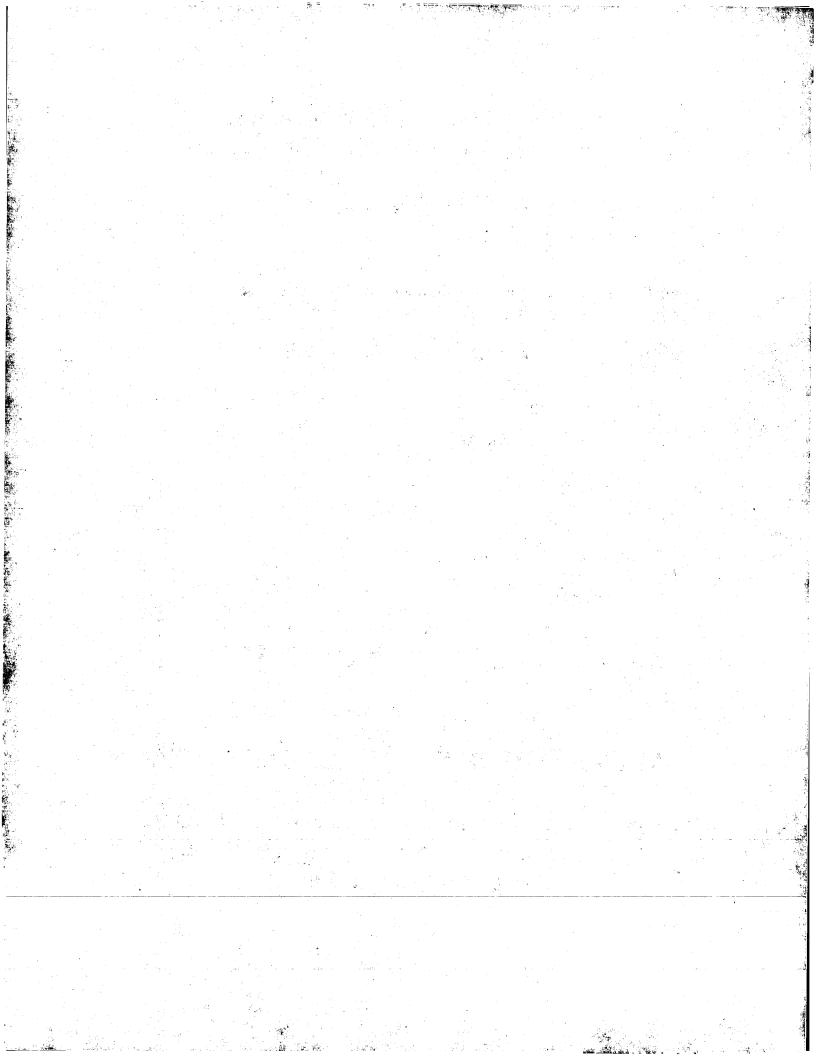
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(71) Applicant: BIOJECT, INC. [US/US]; 7620 S.W. Bridgeport Road, Portland, OR 97224 (US).

(72) Inventors: PETERSON, Steven, Fisher; 4090 Serango Court, West Linn, OR 97068 (US). ASHLEY, John, Whitsett; 5805 Rood Ridge, Hillsboro, OR 97123 (US). BARTHOLOMEW, Victor, Leon; 9044 S. W. Hill Street, Tigard, OR 97223 (US). CASEY, James, Paul, Sr.; 3356 Lavina Drive, Forest Grove, OR 97116 (US). McKINNON, Charles, Neal, Jr.; 7 Park Paseo, Laguna Niguel, CA 92677 (US).

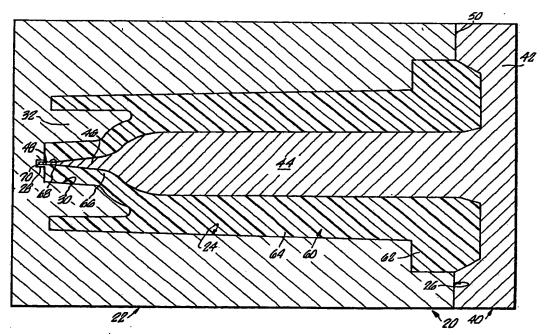
(74) Agents: OHRINER, Kenneth, H. et al.; Lyon & Lyon, 611 West Sixth Street, 34th Floor, Los Angeles, CA 90017 (US).

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(54) Title: METHODS AND MOLDS FOR MANUFACTURING AN AMPULE



A method and mold for making an ampule (60) for a needleless or jet injector device. The tip (48) of a cor pin (40) is guided into a clearance hole (28) sufficiently large to prevent the tip from hitting the mold cavity (22). Plastic is injected into the mold (20) and flows into the space between the core pin tip (48) and the clearance hole (28) forming a vestigial nozzle pilot cylinder (70) around and over the ampule nozzle (68). The ampule (60) is removed from the mold (20) and the vestigial nozzle pilot cylinder (70) is removed to form a finished ampule. A core pin tip is made of drawn wire or is separately replaceable on the core pin. A nozzle of an ampule is cast in place. An ampule is molded with an enlarged nozzle and a separate orifice is installed in the ampule to provide the desired nozzle opening.

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DESCRIPTION

Methods And Molds For Manufacturing An Ampule

Background of the Invention

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Needleless or jet injectors typically use pressurized gas to accelerate a plunger into an ampule holding liquid injectant, thereby causing the injectant to flow out of the ampule with sufficient pressure or velocity to penetrate the skin of the patient. Ampules used with needleless injectors are preferably disposable, must be strong enough to withstand the stresses of injection, and must be made from a bio-compatible material. In addition, ampules are preferably transparent to allow for visual inspection of their contents.

Thermoplastic injection molding is preferred for manufacturing ampules because there are numerous thermoplastics available which are bio-compatible, strong, and have pood transparent, characteristics. In addition, in a typical injection molding process for manufacturing ampules, an injection cycle can be completed in less than one minute, and multiple molds or cavities allow for proportionally lower costs, a significant factor for disposable ampules. injection molding process also can achieve smooth contours and transitions within the ampule, which provides for more injectant flow during injection. efficient liquid tolerances Sufficient manufacturing can also economically maintained with thermoplastic injection molding, whereas attempting to achieve the same result drilling would difficult. machining orbe with Thermoplastic injection molding also results in ampules free of particulate matter, whereas machining and drilling processes create particles that must be removed in a separate process which increases cost and complexity.

Molds used to produce ampules are generally constructed of two primary elements, a cavity housing and

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a core pin. The cavity housing forms the external surfaces of the ampule, while the core pin forms the internal surfaces, including the critical nozzle section.

Frequently, in thermoplastic injection 5 production of ampules, the core pin tip fractures or breaks during the molding process. Bending stresses on the core pin tip can be introduced when the tip of the core pin is inserted into a pilot hole, as the mold is closed. Bending of the core pin tip also occurs when the hot liquid plastic is injected into the mold. pressure of flowing plastic is not uniform on all sides of the pin, resulting in deformation of the core pin tip. This produces bending fatigue of the tip and eventual breakage.

Breakage also occurs when the mold is opened and the ampule is removed after the molten plastic has solidified. The core pin tip becomes very hot during the injection of the plastic because it is not cooled by water as are other surfaces of the mold. This can result in welding of the plastic to the steel pin tip. Although the preferred ampule molding material, high strength polycarbonate, has good clarity and strength, it unfortunately also sticks to the mold surfaces more than most other plastics.

The force required to shear a welded plastic ampule from a core pin is proportional to the diameter of the pin, while the strength of the pin is proportional to the diameter squared. The stress on the pin during removal of from the mold is therefore ampule proportional to the diameter of the pin. Hence, there is a limit on how small the core pin tip can be before it cannot be withdrawn from the part without breaking, and with smaller diameter core pin tips, the breakage rate is higher. The rate of breakage of the core pin tip is inversely related to the diameter of the ampule nozzle. For ampules having 0.008 inch diameter nozzles, the breakage rate is low and the molding process is reliable enough to produce parts on an ongoing basis. On the other

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hand, for ampules with 0.004 inch diameter nozzles, the breakage rate is very high and mak s the injection molding process not cost effective because the process must be stopped and the mold disassembled and repaired with each core pin tip breakage.

The pilot hole typically has a 0.0015 inch clearance gap around the core pin tip. This very close fit prevents flashing of the plastic into the clearance gap. However, if the core pin tip strikes the edge of the pilot hole during closure of the mold, the tip will bend and/or break. The dimensional control of the pilot hole in the cavity housing-core pin registration in a multiple cavity tool, with thermal distortion, approaches the limits of the current art in mold making and injection molding. Accordingly, there is a need for an improved method for manufacturing ampules.

Summary of the Invention

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The present invention is directed to a tool and methods for manufacturing ampules. To this end, a core pin tip is guided into a clearance hole in the cavity housing that is sufficiently large to ensure that the core pin tip will not hit the side of the clearance hole. The excess cylinder of material formed in the clearance hole during injection of the plastic is cut off to open up the nozzle of the ampule, after the ampule is removed from the mold. The core pin tip can also be made of high strength wire, to resist breakage, or can be made replaceable. Also to the this end, the ampule nozzle may be cast in a secondary operation, or the nozzle can be formed by inserting or attaching a separate orifice to the ampule.

Accordingly, it is an object of the invention to provide improved methods and apparatus for manufacturing ampules.

Brief Description of the Drawings

Other objects and features of the present invention will become apparent from the following detailed description taken in connection with the accompanying drawings, which disclose several embodiments of the invention. It is to be understood, however, that the drawings are designed for the purpose of illustration only and are not intended as a definition of the limits of the invention.

In the drawings, wherein similar reference characters denote similar elements throughout the several views:

Fig. 1 is a section view of the present mold in the closed position;

Fig. 2 is an enlarged section view fragment of the mold of Fig. 1;

Fig. 3 is a section view fragment of a second embodiment of a core pin;

Fig. 4 is a section view fragment of a third embodiment of a core pin;

20 Fig. 5 is an enlarged section view fragment illustrating the present method of casting a nozzle section in an ampule;

Fig. 6 is an enlarged section view of an ampule having a metal orifice forming the nozzle section;

Fig. 7 is a section view fragment of an ampule having a plastic orifice forming the nozzle section;

Fig. 8 is an enlarged section view fragment of a rim orifice on an ampule;

Fig. 9 is an enlarged section view fragment of a cap 30 orifice on an ampule;

Fig. 10 is an enlarged section view fragment of a plug orifice on an ampule; and

Fig. 11 is an enlarged section view fragment of a shoulder orifice on an ampule.

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Detailed Description of the Preferred Embodiments

As shown in Fig. 1 a mold 20 for injection molding an ampule includes a mold cavity housing 22 having tapered inner cylindrical walls 24 and a back or proximal end 26. At the front end or distal end of the mold 20 is a clearance hole 28 concentrically positioned within a nose bore 30 formed by a distal ring 32.

A core pin 40 has a base 42 and a slightly tapered elongate cylindrical body 44. A generally conical core pin neck 46 extends forwardly from the body 44 and tapers down to a cylindrical core pin tip 48. The core pin base 42 and the mold cavity housing 22 come together at a parting line 50.

As shown in Fig. 1 the mold 20 shapes injected thermo-plastic into an ampule 60. The ampule 60 formed by the mold 20 has lugs 62 at the back or proximal end. An ampule body 64 is formed in between the mold cavity housing 22 and the core pin body 44. A throat section 66 of the ampule 60 is formed in between the core pin neck 46 and the distal ring 32.

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Turning to Fig. 2, the core pin tip 48 in combination with the distal ring 32 and clearance hole 28 form a nozzle 68 in the ampule 60. The nozzle 68 is surrounded and occluded by a vestigial nozzle pilot cylinder 70.

In use, the core pin tip 48 is piloted or guided into the clearance hole 28 which is made sufficiently large to prevent the core pin tip 48 from hitting the sides of the clearance hole 28 during closure of the mold, as well as during injection of the plastic. Injected plastic flows into the space between the core pin tip 48 and the clearance hole and forms the vestigial nozzle pilot cylinder 70 at the front of the ampule. The ampule is removed from the mold. In a secondary cutting operation, the nozzle pilot cylinder 70 is cut off, thereby exposing the nozzle 68 and producing a finished ampule. The cost of cutting off the nozzle pilot cylinder 70 to expose the nozzle 68 is low and does not significantly add to the

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cost of the final ampule. This mold and molding method helps to prevent breakage of the core pin tip 48 by avoiding the need to pilot the core pin tip into a tight-fitting pilot hole in the mold cavity housing 22.

Fig. 3 shows a core pin 80 constructed with a tip 82 of drawn wire which is welded to the core pin 80. The drawn wire tip 82 has very high tensile strength and is less susceptible to breakage from bending because it is less brittle than a machined core tip. The wire core pin tip also allows use of core pin materials other than tool steel that have improved strength characteristics that elevated temperature, such as tungsten wire. The core pin 80 may be used in a conventional ampule mold, i.e., a mold having a very close clearance pilot hole, or it may also be used in the mold 20 as shown in Fig. 1, or as shown in Fig. 2.

Turning to Fig. 4, a core pin 86 has a threaded hole 90 at its flat distal face 96. A replaceable core pin tip has a threaded stud 92 engageable into the threaded hole 90 in the core pin 86. A flat shoulder 94 seats flush against the flat distal face 96 of the core pin 86, to form a smooth uninterrupted core pin neck. The core pin shown in Fig. 4 may be used in a conventional ampule mold or in the mold 20 shown in Fig. 1.

Fig. 5 illustrates a mold and method for casting an ampule nozzle in a secondary operation. An ampule 100 has a cup opening 102 at its distal end where the nozzle ordinarily would be located. The cup opening 102 is molded into the ampule 100. After molding, the ampule 100 is ejected or removed from the mold. A tapered pin 106 having pin tip 108 that matches the desired nozzle size and shape is inserted into the cup opening 102 from the proximal end of the ampule. Casting material 104 is introduced into the cup opening 102 and is solidified or cured. The tapered pin 106 is withdrawn leaving a cast nozzle. This mold and method allows the ampule 100 to be molded at low cost and without tool breakage. The casting

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material may use any one of several biocompatible materials such as urethane, epoxy or ultraviolet cured materials. The casting material 104 and the material of the tapered pin 106 are selected to provide good release of the tapered pin 106 from the casting material 104 to avoid breakage of the pin tip 108 due to sticking when the tapered pin 106 is withdrawn. This casting operation may be automated to lower manufacturing costs.

Referring to Figs. 6 and 7, with another tool and method, an ampule body is molded with an enlarged opening at its distal end, at the nozzle location, and a separate orifice is installed in a secondary operation which can be automated for low cost. This method allows the ampule body to be molded at low cost without tool breakage, yet still provide the desired nozzle configuration.

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As shown in Fig. 6, an ampule 110 is molded with an oversize nozzle 114. An orifice 112 made of formed stainless steel is installed into the oversize nozzle 114 from the proximal or back open end of the ampule 110. The metal orifice 112 is held in place and made leak free by press fitting and the wedge geometry of the oversize nozzle 114.

As shown in Fig. 7, an ampule 116 has an oversize nozzle 117 and a plastic material orifice 118 is press fit into the oversize nozzle 117 from the proximal end of the ampule 116. A shoulder 119 secures the plastic orifice 118 in position.

Preferably, the orifice 118 is made of a plastic that does not stick to tooling as severely as polycarbonate. High strength is not an important criteria in the nozzle section of the ampule because the diameter of the nozzle opening is much less compared to other diameters of the ampule, resulting in less stress on the material during injection. In addition, because the molded plastic orifice 118 is small in size, dimensional control of the pilot hole/core pin registration in the mold (for making the orifice 118) and the molding process is more easily

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accomplished to allow the pin to be piloted into a pilot hole without striking the edge of the pilot hole. Furthermore, the core pin used in molding the orifice 118 will not deform as much during the injection of the plastic into the orifice mold because the pin is much shorter. This helps to prevent breakage of the pin tip. Molding the orifice 118 as a separate piece allows for use of a single ampule body design that can accommodate various separate orifices, to provide different nozzle 10 shapes and diameters. Molding of the orifice 118 as a separate piece can be accomplished at low cost because the small size of the part allows it to be molded in a mold having a large number of cavities (yet still at low cost) and have very fast molding cycle times.

As shown in Fig. 8 an ampule 120 has a rim orifice 122 attached at its distal end to form a nozzle 123. The rim orifice 122 has a T-shaped cross section.

Turning to Fig. 9, a cap orifice 126 is attached at the distal end of an ampule 124 to form a nozzle 125.

As shown in Fig. 10, an ampule 128 is provided with a plug orifice 130 forming a nozzle 131. The separate orifices 122, 126 and 130 in Figs. 8-10 may be bonded to the complimentary external surfaces of the ampules using adhesives, solvents, sonic welding, heat staking, and 25 other plastic bonding methods.

Turning to Fig. 11, a shoulder orifice 134 is heat staked at the distal end of an ampule 132 forming a nozzle 133.

Thus, while several embodiments and applications of the invention have been shown and described, it would be apparent to those skilled in the art that many more modifications are possible without departing from the inventive concepts herein. The invention, therefore, is not to be restricted except in the spirit of the appended 35 claims.

Claims

1. A method of molding an ampule comprising the steps of:

guiding a core pin tip into a clearance hole in a mold cavity housing;

injecting plastic into the mold cavity housing and allowing the plastic to flow into the clearance hole and around the core pin tip;

allowing the plastic to at least partially solidify

10 and form a nozzle pilot cylinder around the tip of the

core pin;

withdrawing the tip of the core pin from the clearance hole;

removing the ampule from the mold cavity housing; and removing the nozzle pilot cylinder from the ampule to form a nozzle opening in the ampule.

- 2. The method of claim 1 wherein the plastic is polycarbonate.
- 3. A mold for molding plastic ampules comprising: a mold cavity housing;
- a core pin positionable at least partially within the mold cavity housing; and
- a drawn wire attached to an end of the core pin to form a wire core pin tip.
- 25 4. The mold of claim 3 wherein the drawn wire comprises a tungsten wire.
 - 5. A mold for molding plastic ampules comprising: a mold cavity housing;
- a core pin positionable at least partially within the 30 mold cavity housing;
 - a replaceable core pin end; and

means for attaching the replaceable core pin end to the core pin.

6. The mold of claim 5 wherein the means for attaching comprises screw threads.

7. A method of manufacturing an ampule having a nozzle at its distal end and an open proximal end, comprising the steps of:

molding the ampule with a cup recess around an opening in the face of the distal end of the ampule;

inserting a pin through the opening and into the cup recess, from the proximal end of the ampule;

introducing a casting material into the cup recess; solidifying the casting material; and withdrawing the pin.

- 8. The method of claim 7 wherein the pin is tapered.
- 9. The method of claim 7 wherein the casting material is a material selected from the group consisting of urethane, epoxy and ultraviolet curable materials.
- 10. A method of manufacturing an ampule having a nozzle at its distal end and an open proximal end, 20 comprising the steps of:

molding an ampule with an enlarged opening on its distal end; and

installing an orifice in the enlarged opening, from the proximal end of the ampule.

- 25 11. The method of claim 10 wherein the orifice is generally funnel shaped.
 - 12. The method of claim 10 wherein the orifice is stainless steel.
- 13. The method of claim 10 wherein the orifice is 30 installed by press fitting.

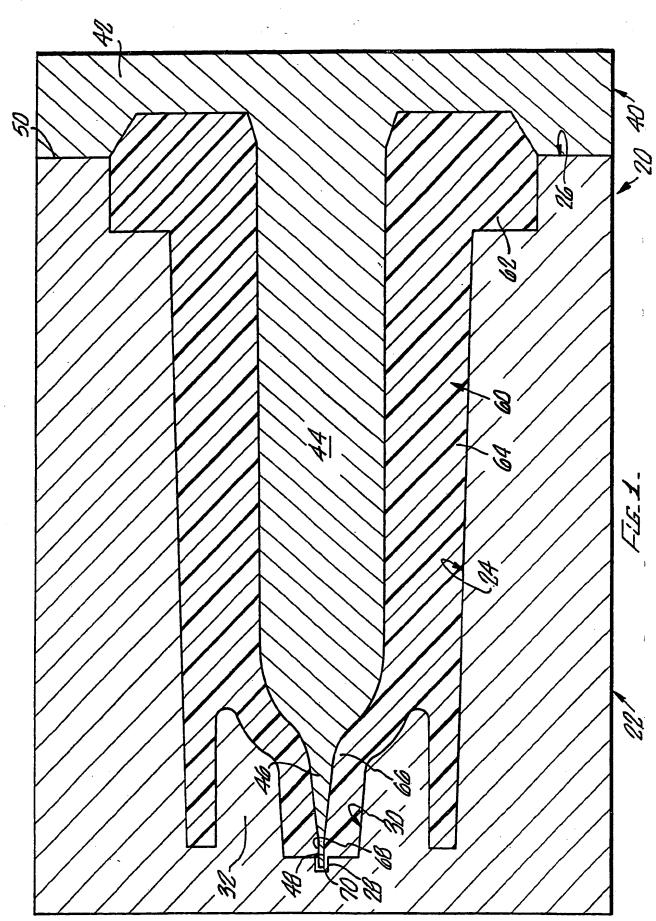
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- 14. The method of claim 10 wherein the orifice is plastic.
- 15. The method of claim 14 wherein the plastic is polycarbonate.
- 5 16. A method of manufacturing an ampule having a nozzle at its distal end, comprising the steps of:

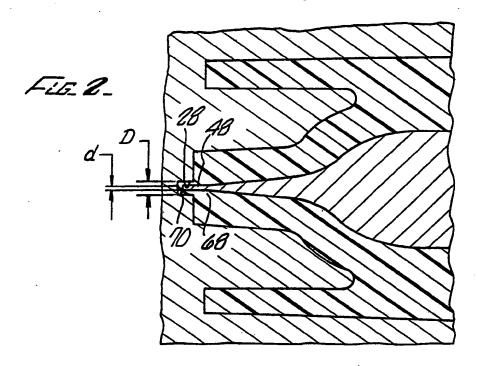
molding an ampule with an enlarged opening on the distal end; and

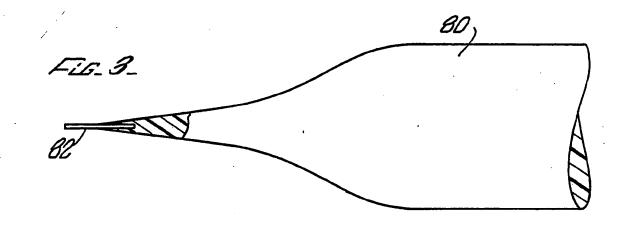
attaching an orifice onto the enlarged opening.

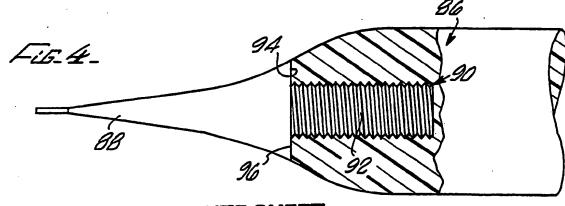
17. The method of claim 16 wherein the orifice is attached to the opening on the ampule using a joining technique selected from the group consisting of adhesives, solvents, sonic welding and heat staking.



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SUBSTITUTE SHEET

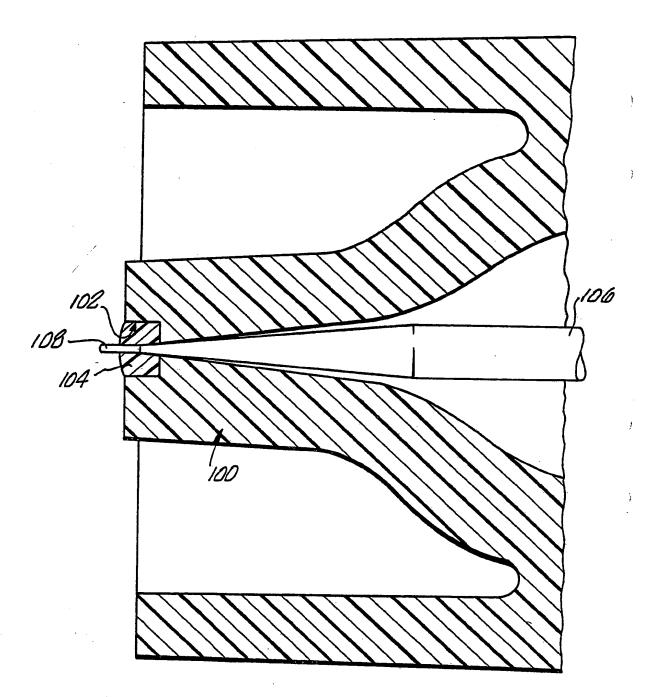
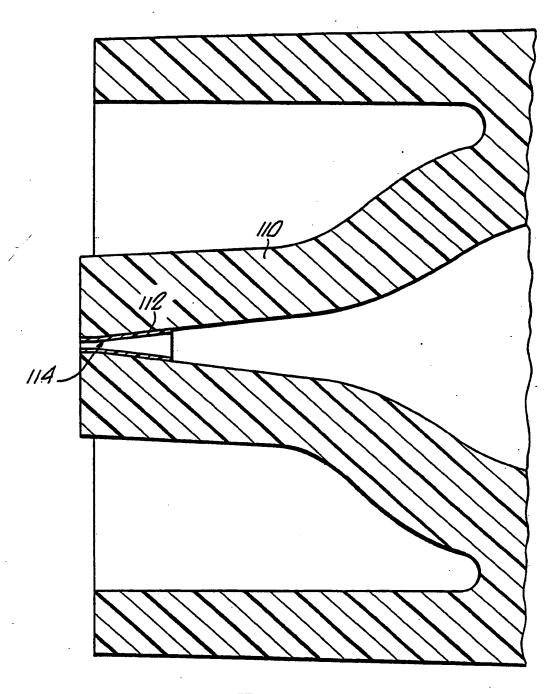


Fig. 5_ SUBSTITUTE SHEET



Fis.6.

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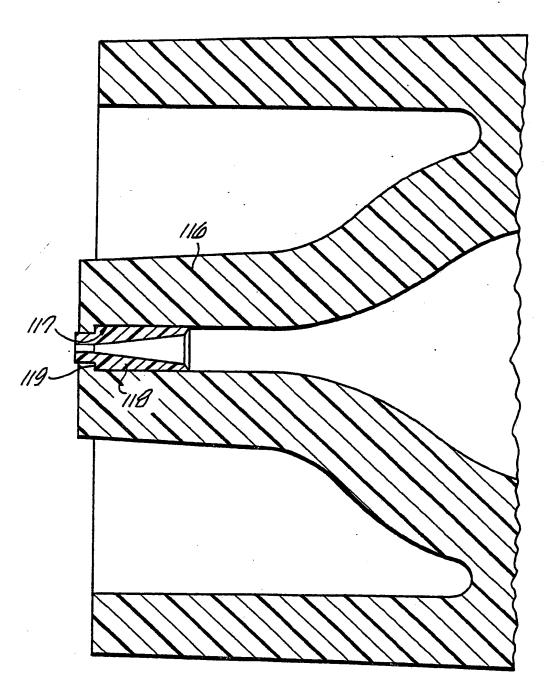
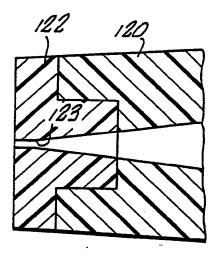


FIG. 1.
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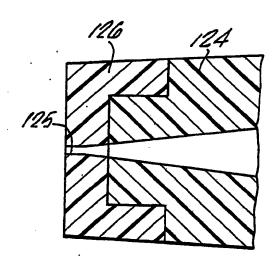
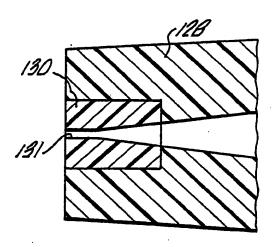


Fig. 9.



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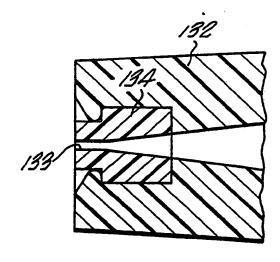


Fig. 11.

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International application N . PCT/US93/04250

A. CLASSIFICATION OF SUBJECT MATTER							
IPC(5) :B29C 39/10, 45/00, 65/00 US CL :Please See Extra Sheet.							
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Electronic d	ata base consulted during the international search (na	me of data base and, where practicable,	search terms used)				
C. DOC	UMENTS CONSIDERED TO BE RELEVANT		1				
Category*	Citation of document, with indication, where ap	propriate, of the relevant passages	Relevant to claim No.				
A	US, A, 2,087,470 (Davidson et al)	20 July 1937.	1-2				
Y	US, A, 2,387,034 (Milano) 16 Oc 39-48.	tober 1945, col. 1, lines	1-6				
Y	US, A, 3,855,380 (Gordon et al) 17 1, 2, and 8, col. 4, line 39 -col. 5,	1-6					
Y	US, A, 4,126,291 (Gilbert et al) 2: lines 11 and 12, and Abstract.	1-6					
Y	US, A, 4,649,616 (Bricker) 17 March 1987, Abstract and 3-6 Figures 9-11.						
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Form PCT/ISA/210 (second sheet)(July 1992)*

International application No. PCT/US93/04250

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim N	
Y	US, A, 3,945,383 (Bennett et al) 23 March 1976, col. 1, lines 53-68.	1-17	
Y .	US, A, 4,925,128 (Brody) 15 May 1990, col. 2, lines 43-61.	10, 13, 14, 16	
.	US, A, 5,078,690 (Ryan) 07 January 1992, col. 2,line 67-col. 3, line 3.	16, 17	
7	US, A, 2,737,946 (Hein) 13 March 1956, col. 2, lines 39-48.	10-17	
\	US, A, 4,284,459 (Patel et al) 18 August 1981.	7-9	
7	US, A, 4,956,903 (Thuries) 18 September 1990, Figure 2C.	11	
	US, A, 3,013,308 (Armour) 19 December 1961, Figures 11-13.	10,11,13,14,15,1 6	
.,Р	US, A, 5,135,599 (Martin et al) 04 August 1992.		
	US, A, 4,838,881 (Bennett) 13 June 1989.		

Form PCT/ISA/210 (continuation of second sheet)(July 1992)+

International application No. PCT/US93/04250

Box	x I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)
	international report has not been established in respect of certain claims under Article 17(2)(a)-for the following reasons:
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2. [Claims Nos.: because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
3. [Claims Nos.: because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).
Box I	I Observations where unity of invention is lacking (Continuation of item 2 of first sheet)
This I	International Searching Authority found multiple inventions in this international application, as follows: (Telephone Practice) Please See Extra Sheet.
1. X	As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2.	As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
· [As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
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· 🗆	No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:
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emark	n Protest The additional search fees were accompanied by the applicant's protest. No protest accompanied the payment of additional search fees.
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Form PCT/ISA/210 (continuation of first sheet(1))(July 1992)*

International application No. PCT/US93/04250

A. CLASSIFICATION OF SUBJECT MATTER: US CL:

264/154, 238, 255, 259, 267, 328.1; 206/528; 29/428, 455.1; 156/245, 294

B. FIELDS SEARCHED

Minimum documentation searched Classification System: U.S.

264/154, 161, 162, 238, 245, 246, 248, 249, 255, 259, 267, 268, 328.1; 206/528; 29/428, 455.1; 156/245, 294; 249/149; 425/577, 468; 604/232

BOX II. OBSERVATIONS WHERE UNITY OF INVENTION WAS LACKING This ISA found multiple inventions as follows:

Claims 1-6, drawn to a first process and first apparatus, classified in Class 264/154.

II. Claims 7-9, drawn to a second process, classified in Class

Claims 10-17, drawn to a third process, classified in Class

264/255

Group I features injection molding and removing the pilot cylinder which is not in Groups II and III.

Group II features casting material in a cup recess which is not in Groups I and III.

Group III features installing or attaching an orifice to an enlarged opening which is not in Groups I and II.

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